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C ABAQUS User subroutine UMAT
C The subroutine implements graded elements with variable Young's
C modulus and Poisson's ration in accordance with Mori-Tanaka
C scheme into ABAQUS/Standard.
C The subroutine handles for 3-D problems.
C
C If using this code for research or industrial purposes, please
C cite: Vycheslav N. Burlayenko & Tomasz Sadowski, Free vibrations
C and static analysis of functionally graded sandwich plates with
C three-dimensional finite elements, Meccanica (2019)
C
C NOTE: FGM PLATE with material gradation through-the-
C thickness. HERE it means through the Y-axis
C
      SUBROUTINE UMAT(STRESS, STATEV, DDSDE, SSE, SPD, SCD,
1  RPL, DDSDDT, DRPLDE, DRPLDT, STRAN, DSTRAN,
2  TIME, DTIME, TEMP, DTEMP, PREDEF, DPRED, MATERL, NDI, NSHR, NTENS,
3  NSTATV, PROPS, NPROPS, COORDS, DROT, PNEWDT, CELENT,
4  DFGRD0, DFGRD1, NOEL, NPT, KSLAY, KSPT, KSTEP, KINC)
C
      INCLUDE 'ABA_PARAM.INC'
C
      CHARACTER*80 MATERL
      DIMENSION STRESS(NTENS), STATEV(NSTATV),
1  DDSDE(NTENS,NTENS), DDSDDT(NTENS), DRPLDE(NTENS),
2  STRAN(NTENS), DSTRAN(NTENS), TIME(2), PREDEF(1), DPRED(1),
3  PROPS(NPROPS), COORDS(3), DROT(3,3),
4  DFGRD0(3,3), DFGRD1(3,3)
C
      LOCAL ARRAYS
C
      DIMENSION EELAS(6), ETHERM(6), DTHERM(6)
C
      PARAMETER (ZERO=0.00, ONE=1.00, TWO=2.00, TWOTHIRD=2.00/3.00,
1  HALF=1.00/2.00, THREE=3.00, FOUR=4.00, FOURTHIRD=4.00/3.00)
C
      REAL*8 E, NU, MU, LAMBDA, PHAS, AKM, AKC, AGM, AGC, FUM, AKE, AGE
C
      DATA THICKNESS, VOLC /50.000,1.000/
C
      DETERMINNE MATERAILS PROPERTIES BASED ON GLOBAL COORDINATES
IN GAUSS POINTS.
C
      COORDS(1)  is  X-coordinate of  Gauss points.
      COORDS(2)  is  Y-coordinate of  Gauss points.
      COORDS(3)  is  Z-coordinate of  Gauss points.
C
      USER SPECIFY PARAMETERS FOR THE SUBROUTINE
C
      PROPS(1) IS Em : Young's modulus of metal on bottom surface
      PROPS(2) IS Ec : Young's modulus of ceramic on top surface
      PROPS(3) IS p  : the exponent
      PROPS(4) IS NUm : Poisson's coefficient - constant
      PROPS(5) IS NUc : Poisson's coefficient - constant
C

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C      CHANGE FOR NEW PROBLEM
C      PHAS = ZERO + VOLC*(HALF + COORDS (2) /THICKNESS)**PROPS (3)
C
C      BULK MODULUS
C      AKM = PROPS (1) /THREE/ (ONE-TWO*PROPS (4) )
C      AKC = PROPS (2) /THREE/ (ONE-TWO*PROPS (5) )
C      SHEAR MODULUS
C      AGM = PROPS (1) /TWO/ (ONE+PROPS (4) )
C      AGC = PROPS (2) /TWO/ (ONE+PROPS (5) )
C      FUM=AGM*(THREE*THREE*AKM+FOUR*TWO*AGM) /THREE/TWO/ (AKM+TWO*AGM)
C
C      EFFECTIVE MATERIAL PARAMETERS
C      AKE = AKM + (AKC-AKM)*PHAS/(1 + (1-PHAS)*(AKC-AKM)/(AKM +
C      1 FOURTHIRD*AGM))
C      AGE = AGM + (AGC-AGM)*PHAS/(1 + (1-PHAS)*(AGC-AGM)/(AGM +
C      1 FUM))
C
C      E = THREE*THREE*AKE*AGE/(THREE*AKE+AGE)
C      NU = (THREE*AKE-TWO*AGE)/TWO/(THREE*AKE+AGE)
C
C      DETERMINE THE LAME'S CONSTANTS
C
C      MU=E/TWO/(ONE + NU)
C      LAMBDA=E*NU/(ONE+NU)/(ONE-TWO*NU)
C
C      DETERMINE THE TANGENT(JACOBIAN) MATRIX
C
C      NDI IS NUMBER OF NORMAL STRESSES:  SXX, SYX, SZZ
C      NSHR IS NUMBER OF SHEAR STRESSES:  SXY
C      NTENS IS DIMENSION OF CONSTITUTIVE MATRIX,NTENS=NDI + NSHR
C
C      DO I=1,NDI
C        DO J=1,NDI
C          IF (I.EQ.J) THEN
C            DDSDE(I, I)= LAMBDA + TWO*MU
C          ELSE
C            DDSDE(I, J)= LAMBDA
C          ENDIF
C        ENDDO
C      ENDDO
C
C      DO I=NDI+1,NTENS
C        DDSDE(I, I)= MU
C      ENDDO
C
C      DETERMINE THE STRESS AND UPDATE THE STRESS
C
C      DO I=1,NTENS
C        DO J=1,NTENS
C          STRESS(I)=STRESS(I) + DDSDE(I, J)*DSTRAN(J)
C        ENDDO
C      ENDDO
C
C      RETURN
C      END

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